DERIVATOGRAPHIC INVESTIGATIONS INTO THERMAL DECOMPOSITION OF DISPERSED PARTICLES OF METAL-CARBON COMPOSITES

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Introduction

One of the main obstacles in the prolonged reversible use of hydride-forming alloys is their poisoning with electronegative impurities (O,N etc.).

In the course of cycling these impurities arrange on the crystallite surface and take some area on the grain boundaries. This complicates hydrogen diffusion into the crystallite bulk and back and slows down the time for charge-discharge processes. The large accumulation of these impurities (mainly as oxides and oxynitrides) results in the material dispersion, difficulty in heat and mass transfer. Moreover, in some alloys and intermetallic compounds, with increasing temperature, oxygen and nitrogen diffusion along the grain boundaries alternates by volume diffusion of these elements. As a result, the number of interstices capable of placing hydrogen is decreased what leads to the sharp decrease in the material hydrogen capacity [1-23].

We have attempted to prepare the metalcarbon composite in the form of ultradispersed powder of hydride-forming alloys. The surface of particles in these alloys was covered with the thin layer of nanostructural carbon. The nanostructural carbon layer is thought to be penetrable for hydrogen and impenetrable for electronegative impurities.

In this work the investigations into interaction of dispersed powders of metal-carbon composites with air atmosphere are presented. Investigations have been performed in heating from the room temperature to 1000 °C on Q-1500D derivatograph.

Fig.1 shows the following particles: a - initial particle with a carbon layer; b - after treatment for 1 min by ultrasound. The chip in the piece of the layer is seen.

Table 1. (Values of Temperatures are given in °C)

	Material	Temperature DTG					DTA	Change	Temperature
N		of beginning the change in mass	T ₁ max	T ₂ max	T ₃ max	T ₄ max	Tmax	in mass	range of thermal decomposition
1	Nickel produced in alcohol	230	280				280	-8	230 — 400
2	Nickel produced in toluene	240	310	330	340		345	-24	240 — 400
3	Nickel produced in solvent-2355	240		330	340		340	-23	240 — 460
	Nickel produced in solvent 2355, additionally purified in toluene	235	310	325			325	-29	235 — 410
5	LaNi ₅ , produced in toluene	240	310	330			340	-33	240 — 430
6	LaNi ₅ , produced in solvent-2355	270		330	340		350	-24	270 — 460
	LaNi ₅ , produced in solvent 2355, additionally purified in toluene	240	310		340		330	-41	240 — 440
	LaNi ₅ , produced in toluene and purified by ultrasound	240		325			330	-44	240 — 430
	Dispersed carbon produced in toluene	210	340	420	500	710	710	-98	210 — 740
	Dispersed carbon produced in toluene and treated by ultrasound	250	250	550	630	648	648	-98	250 — 680
11	Nickel electrolytic	280	550	660				23	280-750
	LaNi ₅ powder produced by mechano-chemical method	280	550				550	45	280-840

Experiment and results

The following composites have been studied: powders of pure nickel and LaNi₅; dispersed powders of nickel and LaNi₅ produced by the electric spark method in toluene, alcohol, solvent-2355 - unpurified powders and powders purified in pure toluene; powders additionally purified using ultrasound in pure toluene; dispersed powder of spectro-pure carbon.

On the base of the study performed the following has been found: temperature ranges for thermal decomposition of dispersed powders, values of mass loss in heating (due to the evolution of different gases), temperatures for maximum rates of mass loss. The difference-thermal analysis has been performed (Table 1).

It has been found that depending on the powder composition, the technique for its preparation and purification, the temperature for the beginning process of mass loss and the range of its occurrence are different.

Conclusions

The value of mass loss significantly differs for different powders. The experiments performed have allowed us to outline the ways for further investigations directed at the creation of metal-carbon hydrogensorbing materials with the enhanced cyclic stability.

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